1394

	Pg.
X Sects of Miller Borrow Pit	42-43.
X Sects of Markeley Borrow Pit	47-48
Line along Riverside Road	52
X Sects on Riverside Road	53-54.
X Sects of Proposed Site of Freeport Wharf	57-58
" " " " " Depot	59.
" " " Borrow Pit sta. 338+65 to 349+80	63 to 67

1395

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X Secs: of Road approach to "Y" St adjoining Mr Pierce's Property.	20
X Secs of Approach to "Y" St on West for City of Sacramento	21.
X Secs: opp: Retaining Wall at Gas Works	24.
X Secs of Merkley Borrow Pit	26-27
X Secs on Co: Road Sta: 149+60.	30.
X Secs of Slough at Klotz Ranch	31.
Orig: X Sec: of Miller Borrow Pit	32-33
X Secs of Same for November Estimate	42-43
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X Secs. opp. Retaining Wall at Gas Works	24.
X Secs. of Merkeley Borrow Pit	26-27.
X Secs. on Co. Road Sta. 149+60	30.
X Secs. of Slough at Klotz Ranch	31.
Orig X Secs. of Miller Borrow Pit.	32-33.
X Secs. of County Road South of "Y" St.	37 to 40

(OVER.)

1396

Sta.	Ground	Grade					
			L.		C.	R.	
X123		19.976	-0.4 9.6	-0.4 9.0	-0.5	-0.4 9.	-0.4 9.6
X123 + 50		21.972	-3.3 14.0	-3.4 9.	-2.9	-3.0 9.	-2.8 13.2
X124	3.89	23.869	-5.3 17.0	-5.2 9.	-4.9	-4.8 9.	-4.7 16.0
X124 + 50		25.816	-7.3 20.0	-7.5 9.	-7.3	-7.0 9.	-7.3 20.0
X125		27.762	-9.6 23.4	-9.4 9.	-9.4	-9.2 3.5	0.0 17.7
X125 + 50	3.89	29.708	-12.2 27.3	-11.8 9.8	-5.2	0.0 7.8	
X126		31.655	-14.6 30.9	-14.6 20.4	-0.7	0.0 1.0	
X126 + 33.37		32.954	-16.0 32.0	-15.9 25.	-5.5 8.3	0.0 0.7	0.0
X126 + 63.37	30		-16.2 33.3	-16.3 28.5	-3.5 4.7	0.0 4.3	0.0
H.B.				0.0 9.0		0.0	0.0 9.0

Sta. Ground Grade. L. C. R. May 14/07

X LINE Riverside Road

2

Calculated
A.W.B.

X121						
X121 + 50			0.0 / 10.	0.0	0.0 / 0.0	
X121 + 94.1	0 15.850					
X122	16.083		+3.2 / 13.2	+3.1 / 2.5	+1.4	+2.2 / 10.	+2.2 / 12.2
X122 + 50	18.030		+1.5 / 11.5	+1.7	+1.3 / 7.8	0.0 / 10.0
122 + 91			0.0 / 10.0	0.0	0.0 / 10.0

+2.893

-3.803

X Sec. of Dump built by Verney Bros.

5.

Sta.	Pro.	Prod							
339			-16.2 33.3	-7.9 20.	-6.6 9.	-7.1	-7.3 9	-8.3 19.	-16.3 33.4
+50			-16.6 33.9	-6.3 16.	-5.7 9.	-6.2	-7.2 9.	-8.5 20	-16.6 33.9
338			-16.7 34.0	-7.6 19.	-8.1 9	-9.6	-10.4 9.	-11.9 23.	-16.8 34.2
+50			-16.8 34.2	-9.7 23.	7.3 17.	-7.0 9.	-7.3	-8.3 9.	-8.9 21	-16.9 34.4
337			-16.8 34.2	-10.9 25.	-7.0 5	-6.9 9.	-7.5	-8.2 9.	10.3 25.5	-16.9 ✓ 34.4
+50			-16.6 33.9	-5.2 14.	-5.3 9	-6.2	-7.6 9.	-9.9 23.	-17.1 ✓ 34.6
336			-16.9 34.4	-7.3 20.	-3.9 9.	-2.7	-4.0 9.	-6.3 18.	-17.3 ✓ 35.0
335+57			-17.0 34.5	-14.0 28	-12.9 26.	-9.3 21.	-7.3 9.	-8.0	-8.8 9.	-10.1 20.5	-17.3 ✓ 35.0
335											Time 7/07

Calculated
EWR.

1399

X Sec. of Carney Bros Dump June 7/07

L C R

6.

+50	-15.1 31.6	-3.4 13.	-3.0 9.	-2.8	-3.6 9.	-4.8 16.	-15.5 32.2
343	-15.2 31.8	-5.3 16	-3.0 9	-2.9	-3.1 9.	-4.8 17	-15.6 32.4
+50	-14.9 31.4	-3.8 13.	-2.5 9.	-2.7	-2.5 9.	-3.8 13.	-15.5 32.2
342	-14.8 31.2	-8.5 20.	-7.9 9.	-8.2	-8.3 9.	-8.5 32.5	-15.3 32.0
341 + 65	-14.8 31.2		-14.9 9	-14.9	-15.0 9		-15.3 32.0

+50	-14.6 30.9		-15.0 9	-15.0	-15.1 9		-15.2 31.8
+18.	-14.6 30.9		-14.9 9	-14.8	-15.0 9		-15.7 31.8
341	-14.5 30.8	-8.8 21.	-8.2 9.	-8.6	-8.5 9.	-10.6 23.	-15.4 32.1
+50	-14.5 30.8	-4.7 13	-4.7 9	-6.1	-6.7 9.	-7.7 19.5	-15.8 32.7
340	-15.0 31.5	-5.3 13	-5.1 9.	-5.0	-5.5 9	-6.7 18.5	-15.7 32.6
339+50	-15.5 32.2	-6.3 14.	-6.3 9	-7.3	-8.2 9	-9.5 22.	-16.0 33.0

1400

X Sec of Carney Bros. Dump June 7/07. 7.

	L.	C.	R					
+50	-13.8 28.2	-4.6 15.	-2.9 9.	-3.0	-3.9 9.	-6.0 17.	-12.9 28.9	
348	-13.1 28.6	-3.0 12.	-2.1 9.	-0.9	-1.0 9.	-2.9 14.	-13.7 28.0	
+50	-13.3 29.0	-3.8 15	-1.2 9	-1.1	-2.9 9.	-4.9 13.5	-12.9 28.4	
347	-13.4 29.1	-4.7 16.	-1.2 9.	-0.5	-2.3 9.	-2.8 12.	-13.2 28.8	
+50	-13.7 29.6	-4.3 15.	-2.2 9.	-2.8	-4.4 9.	-5.2 14.5	-13.2 28.8	
346	-14.3 30.4	-5.0 17.	-1.5 9.	-1.1	-1.8 9.	-3.3 14.	-14.3 30.4	
+50	-14.6 30.9	-5.6 18.	-1.5 9.	-1.5	-1.7 9.	-3.9 15.5	-14.7 31.0	
345	-14.8 31.2	-6.8 19.	-2.4 9	-2.6	-2.6 9.	-3.8 14.5	-14.7 31.0	
+50	-15.0 31.5	-5.3 17.	-3.1 9	-3.2	-3.5 9.	-3.8 13	-5.5 18.	-14.9 31.4
344	-15.0 31.5	-5.8 16.	-5.5 9.	-6.5	-6.9 9.	-8.0 17.5	-15.1 31.6	

1401

X Sec. of Carney Bros Dump June 7/07 8.

L. C. R.

Calculated by O.P.C.

352 + 50	orig: X. Section								
352.	-13.0 28.5	-13.2 27	-13.8 9	-12.3 4	-12.3	-10.6 9.	-11.7 34.	-12.6 27.9	
351 + 66.8									
351 + 64.2									
+ 50	-13.9 29.9	-14.0 12	-12.6 9.	-10.4	-10.8 9.	-11.3 30.5	-12.7 28.0		
351	-14.3 30.4	-14.3 17.	-12.7 14.	-12.2 9.	-10.4	-10.6 9.	-10.8 20.	-12.8 28.2	
+ 50	-14.2 30.3	-14.3 24	-13.5 20.	-12.2 13.	-11.0 9.	-10.7	-10.8 9.	-12.0 24	-13.1 28.6
350	-14.5 30.8	-12.5 25.	-7.5 14.	-7.9 9.	-8.2	-8.4 9	-9.4 19.4	-12.0 26.5	-13.0 28.5
+ 50	-13.9 29.9	-6.7 13	-6.8 9.		-7.1	-7.2 9.	-7.8 16.5	-13.0 28.5	
349	-13.8 28.2	-9.0 13.	-3.7 9		-3.0	-3.2 9.	-4.2 14.5	-12.9 28.4	

* This will probably be East of Grading from borrow pit. That is from Sta 335+57 to Sta 350+50.

47.4 Short Station

S/2.

Secs. taken from W. M. Line as Zero.

X Sec. Borrow Pit Carney.

12.

336.	10.4	9.2	7.0	5.8	5.5	5.4	5.3	6.4	8.7	10.6
	2	6.5	14.	40.	70.	100.	107.	109.	112.	113.
335+50	10.0	8.8	8.2	7.8	7.0	6.5	6.8	7.6	10.3	
	5	6	30	50.	58.	80.	105.	109.	113.5.	

FINAL X-Sects. for work of Carney Bros, which is also Original X-Sects. for work of Reed Force Work.

For X Secs for Est: of work done by Reed.
See pp: 63 - 67.

1403.

Pages 12 To 17 Used In
Final Estimate Item No 72,
and 73. and 75.
and 76.

Secs. taken from R. M. Line July 30/07 13.

S½: for X Sec Borrow Pit

339	FINAL Carney Co.	11.7	9.1	7.6	6.4	5.9	7.9	9.4	11.4
		116.	111.	100.	83.	58.	9.	7.	3.
338 + 84	Original " Reed Co.	15.7	10.4	7.4	5.8	7.4	9.4	11.3	
		127.5	100.	83.	55.	9.	7	3.	
+ 75		15.9	11.3	8.6	7.3	5.9	7.5	9.6	11.2
		126.5	100.	84.	71.	53.	9.	7.	4.
+ 65		11.5	8.8	8.6	7.0	6.0	6.6	7.5	9.6	11.1
		114.0	110.	100.	71.	54.	30.	9.	7.	4.
338 + 50		11.4	8.9	7.1	6.7	5.7	6.3	7.4	11.3
		115.	111.	106.	80.	30.	30.	10.	4
+ 23		11.5	10.1	8.0	6.6	5.5	5.5	6.1	7.2	8.7	11.6
		115.5	112.	100	70.	58.	45.	31	10.	8	4.
+ 11		15.3	13.5	8.1	7.2	5.9	5.9	6.9	9.8	11.4
		127.	112.	85.	73.	54.	30.	11.	7.	3.
338		15.4	11.8	9.3	7.7	5.7	5.9	6.7	9.4	11.1
		125.5	100.	86.	70.	57.	36.	11.	7.	4.
+ 92		11.6	8.6	8.3	7.1	5.6	6.0	6.7	8.8	11.2
		115.0	107.	90.	66.	37.	30.	11.	7.	4
+ 50		11.1	7.9	6.9	5.8	5.0	5.1	5.7	8.9	11.1
		114.	108.	103.	87.	56.	30.	14.	8.	4.
+ 33		11.7	9.4	8.1	5.8	5.1	5.0	5.9	9.0	10.8
		113.	110.	100.	75.	57.	30.	13.	7.	4.
+ 24		15.3	10.6	8.0	6.0	5.1	4.9	5.8	8.6	10.7
		126.	100.	87.	69	55	30.	13.	7.	4.
+ 14		15.7	11.2	8.4	6.5	5.3	5.0	5.5	6.0	8.6	10.6
		126.	100.	83.	65.	50.	30.	18	12.	7.	4.
337		11.0	8.4	8.0	6.4	5.1	5.1	6.0	8.5	10.6
		114.	108.	100.	72.	50.	25.	11.	7.	4.
+ 50.		11.0	9.7	5.5	4.7	4.8	5.0	7.9	10.0
		114.	110.	100	60.	30.	15.	8	5.

Sections taken from R.W. Line July 6/09 14.

S/2: X Sec. Borrow Pits

FINAL for Carney Bros. Work

Original for Reed Co. Work.

+75					12.8 117.	12.0 100.	11.2 60.	9.0 25.	9.4 7.	12.2 2.	
+50						12.6 119.	12.6 100.		12.0 50.	12.3 3.	
341						12.7 116.	11.9 100.	11.8 80.	12.2 40	12.5 2.	
+85				12.6 115.0	11.1 112.	9.6 108.5	9.3 83.	10.0 69.	11.0 42.	12.1 2.	
+68		12.5 114.	10.3 111.5	8.9 108.	7.4 77.	7.7 55.	8.7 30.	9.6 22.	8.8 12.	10.4 6.	11.8 2.
+53				12.4 116.	10.0 111.	8.7 100.	7.3 80.	7.2 33.	7.6 11.	12.0 2.	
+43					15.6 125.5	10.3 100.	7.8 81.	7.3 42.	7.6 10.	11.8 3.	
+33				15.6 127.	10.8 100.	8.5 82.	7.5 64.	7.2 40.	7.5 11.	11.8 3.	
+25				11.7 114.	10.6 111.	9.3 100	8.3 89.	7.1 64	7.1 40.	7.6 10.5	11.9 3.
340		12.7 114.5	10.2 112.	8.9 108.	7.4 86.	7.0 60.	6.7 43.	7.3 14.	7.8 9.	11.8 3.	
+80				12.2 115.	10.3 112.	8.4 100.	6.8 63.	6.4 39.	7.4 10.	11.8 3	
+68				17.1 130.	11.8 100.	9.0 80.	6.9 61.	6.4 36.	7.5 10.	11.8 2.	
+60					17.0 130.	13.0 100.	6.6 60.	6.5 47.	7.6 10.	11.9 3.	
339+50		12.2 116.	10.2 113.	10.1 100.	9.0 84.	6.6 57.	6.1 35.	7.3 28.	7.6 10.	11.8 3.	

Line to N.W.

1405

Soilings taken from R.W. Line

X Secs Borrow Pits

S/2:

+21	12.9	10.0	9.3	9.4	8.9	8.4	9.4	10.8	13.4
	118.	113.	109.	93.	72.	40.	10.	6.	2.
345	13.2	9.9	8.5	8.1	8.6	9.3	12.2	13.4	
	118.	113.	108	100.	38.	11.	5.	3.	
+50	13.2	9.4	7.9	8.0	9.0	10.0	13.0		
	118.	111.	78.	55	12.	2.	3.		
+12	12.9	10.6	9.6	8.1	8.2	8.9	10.7	13.0	
	118.	114.	110.	80.	32.	13.	6.	3	
344	17.2	12.3	11.5	8.5	7.8	8.2	8.8	10.6	13.0
	124.	111.	100	75.	55.	34.	12.	6.	2.
+89	17.5	12.9	8.9	7.6	8.1	8.6	10.0	12.7	
	127.	100.	72.	56.	36.	12	7.	3.	
+73	12.3	9.9	8.9	7.9	8.1	8.4	10.0	12.8	
	117.	112.	85.	60.	30.	14.	6.5	3.	
343+50	12.5	9.2	8.4	7.6	8.0	9.5	12.5		
	117.	110.	100.	40.	15.	7.	2.		
343+05	12.5	9.8	8.7	8.2	7.3	7.3	9.1	12.5	
	117.	111.	100.	84.	54.	19.	6.5	2.	
+92	17.4	12.5	10.4	8.6	7.9	7.3	7.2	8.8	12.3
	127.	111.	100.	84.	63.	55.	13.	6.5	2.
+84	17.0	12.1	10.1	8.6	8.0	7.3	7.0	8.4	12.1
	127.	106.	93.	76.	60.	50.	14.	7.	3.
+73	12.5	10.1	8.6	7.9	7.0	7.0	8.3	12.0
	117.	107.	80.	63.	57.	13.	7.	3.
+50	12.5	10.6	8.8	8.5	8.3	7.7	7.0	7.0	8.3	12.2
	116.	114.	109.	100.	85	70.	59.	14.	7.	2.
342	12.6	9.6	8.5	7.0	7.6	8.7	12.3
	117.0	109.	80.	55.	17.	7.	2.

1406

Sections Taken from R.W. LINE — July 6/07 — 16.

X Secs. Borrow Pits

Station								
348	15.2 / 121.	12.1 / 115.	11.0 / 111.0	10.3 / 100.	9.8 / 50.	9.9 / 21.	11.4 / 10.	14.9 / 6
+ 50	14.9 / 121.	13.2 / 118.	11.1 / 111.	10.4 / 100.	9.4 / 60.	9.8 / 17.	11.1 / 9.	14.9 / 4.
+ 43	18.4 / 133.	15.0 / 120.	11.0 / 105.	9.3 / 60.	10.0 / 15.	11.1 / 9.	14.8 / 4.	
+ 30	18.7 / 133.	15.7 / 127.	13.6 / 116.	10.8 / 105.	10.2 / 87.	9.5 / 62.	9.7 / 8.	11.2 / 8.	14.9 / 3
+ 27	14.9 / 122.5	11.9 / 115.	10.3 / 108.	9.9 / 36.	9.9 / 15.	11.2 / 8	14.9 / 4.	
347	14.8 / 121.	12.3 / 117.	10.1 / 111.	9.4 / 56.	9.4 / 16.	11.3 / 8.	14.5 / 4	
+ 58	14.5 / 120.	11.9 / 115.	10.4 / 100.	9.4 / 30.	9.4 / 17.	10.0 / 10.	14.0 / 3.	

FINAL for Carney Bro. work
Original for Reed. Co. work.

July 28/07.

Station								
+ 43	14.9 / 132.	13.8 / 100.	12.6 / 93.	9.9 / 72.	9.4 / 20.	9.9 / 10.	13.9 / 3.	
+ 34	19.6 / 131.	12.9 / 100	10.9 / 85.	9.7 / 72.	9.4 / 16.	10.1 / 9.	13.8 / 3.	
+ 20.	13.2 / 117.	11.2 / 113.	9.8 / 100.	9.5 / 90.	9.6 / 14.	10.4 / 8.	13.6 / 3	
346	13.5 / 118.	11.9 / 112.	9.7 / 108.	9.3 / 100.	9.1 / 61.	9.0 / 45.	9.8 / 10.	10.8 / 7.	13.8 / 4.
+ 60	12.7 / 116.	10.0 / 110.	9.6 / 100.	8.9 / 60.	8.5 / 47.	9.5 / 10.	10.7 / 7.	13.7 / 3
+ 46	18.2 / 131.	13.5 / 109.	12.9 / 106.	10.0 / 90.	8.9 / 70.	8.7 / 44.	9.6 / 10.	10.9 / 7	13.6 / 3
345 + 36	17.9 / 129.	12.3 / 100.	9.51 / 83.	8.6 / 69.	8.6 / 43.	9.5 / 10.	10.8 / 7.	13.4 / 3.

1407

S/2:

Sections taken from R.R. Line
X-Secs.

FINAL X-Sect. for Carney Bros. Force Work
Original X-Sect. " Reed Co. " "

+ 50	15.0 122.	12.7 117.	12.3 100.	12.4 75	11.4 70	11.7 57	13.6 27	15.5 5.	16.1 2.
349 + 38	15.6 122.0	12.9 118.	12.3 100.	12.5 77.	11.4 64.	11.4 50	14.4 30.	15.3 7.	16.0 3

+ 20	17.5 131.0	15.0 114.	12.7 84.	11.8 57.	11.2 42.	14.5 25	15.2 8.	15.9 4.	
+ 10	14.8 121.5	12.1 116.5	11.6 100.	12.0 75.	11.7 58.	11.3 35.	14.1 21.	15.8 4.	
349	14.9 121.5	12.8 117	11.3 114.	10.5 100.	11.9 68.	11.9 47.	10.9 35	13.3 23.	15.1 14.	15.9 4.
+ 50	14.9 124.	12.7 115.	10.9 100.	9.8 75.	10.9 35.	13.6 11.	15.4 4.		
+ 43	19.2 132.	15.8 118.	11.9 100.	10.4 85.	10.0 60.	10.4 46.	12.0 20.	13.6 10.	15.5 4.
+ 34	19.2 133.	16.5 119.	12.9 100.	10.8 83.	10.2 57.	11.5 30.	13.1 11.	15.0 7.	
348 + 22	15.1 122.	12.7 116.	10.8 90.	9.8 68.	10.7 22.	12.0 11.	15.3 5		

Oct 17/07 20.

X Sections of Road Approach
to "Y" Street adjoining Mr. Pierce's property.
to conform to Miller R.W. Conditions.

18' Wide.
Grade 6.00 per 100.

Sta:	Grade					
2 + 08	19.5	0.0 9.0	0.0	0.0 9.0		
2 + 00	20.0	-0.6 9.9	-0.5 9.	-0.5	-0.4 9	-0.4 9.6
1 + 50	23.0	-3.4 14.1	-3.5 9.	-3.5	-3.3 9.	-3.3 14.0
1 + 00	26.0	-6.7 19.0	-6.6 9.	-6.6	-6.3 9.	-6.3 18.4
0 + 50	29.0	-9.8 23.9	-9.5 9.	-9.4	-9.3 9	-9.0 22.5
0 + 40	29.6	-10.0 24.0	-10.3 9.	-10.2	-10.1 9.	-10.0 24.0
0 + 25	30.5	-6.2 18.2	-6.5 9.	-6.4	-6.5 9.	-6.6 20.4
0 + 00 65' East of E Line	32.0 Crest of Y St Terrace.	0.0 9.0		0.0	0.0 9.0	

Pages 20 To 21 Used In
Final Estimate Item No 20

1409

X Sec of Approach on Y Sheet
West of Sec to Southern. 18' wide
1½-1 Slope

1+60	22.1		0.0 9.0		0.0		0.0 9.0		
1+30	24.5		-1.2 10.8	-1.2 9.	-1.4	-1.5 9.	-1.5 11.2		
1+00	26.9		-5.0 16.5	-5.4 9.	-5.5	-4.1 9.	-2.8 13.2		
0+75	28.9	8.00	-7.6 20.4	-8.4 9.	-7.2	-6.3 9.	-6.0 18.0		
0+50	30.9		-7.1 19.6	-8.8 6.	-5.6	-4.8 5.5	-7.4 9.5	-7.9 19.	-7.1 19.6
0+25	32.9		-5.7 17.6	-5.8 13.	-3.7 4.	-3.6	-2.8 9.	-2.9 13.4	
0+00 = 38+19.2.	34.9			0.0 9.0		0.0		0.0 9.0	

X Sections on River Bank below Freeport.

Mar 30/10.

Sta.

Right

Sta.							
447.	27.0 8	25.2 20.	24.2 42.	24.2 59	20.2 67.	S.W. 16.3 67.5	
446 + 75	27.0 8.	24.4 20.	24.0 38.	24.0 51.5	22.6 54.	17.0 56.	S.W. 16.3 60.
+ 50	27.1 9.	24.1 20.	23.3 38.	23.5 48.	22.9 50.	17.0 53.5	S.W. 16.3 57.
+ 25	27.0 9.	23.9 20.	23.0 51.	16.9 53.	S.W. 16.3 58.		
446	27.1 9.	23.7 20.	22.9 54.5	20.3 61.	16.6 64.	S.W. 16.3 64.5	

*. For extension to these X Secs: taken in River See page 23.

Sta.						
442 + 31	27.1 8.	23.3 20.	23.1 35.	23.1 52.5	18.1 71	S.W. 16.3 72.5
442	27.2 8.5	23.3 20.	23.0 38.	22.9 45.	16.8 49	S.W. 16.3 49.5
+ 50	27.0 8.5	23.3 20.	22.8 38.	21.8 41.	17.1 44.	S.W. 16.3 47.5
441 + 25	26.9 9.	23.1 20.	22.9 39.	21.8 42.	17.0 45	S.W. 16.3 48.5
440 + 85	27.2 9.	22.9 20.	22.5 49.	21.8 59.	17.4 62.	S.W. 16.3 62.5

Sta. X Secs in River below Freeport

Sta.								
447	15.0	14.0	8.0	0.0	-6.0	-9.0		
	73	80	88	100	120	130.		
+75	15.0	12.5	7.0	-2.0	-8.0	-8.0		
	65	75.	85.	100	120.	140.		
+50	15.0	13.0	9.0	5.0	-4.0	-9.0	-10.0	
	62.	77.	80.	90	100	120.	140.	
+25	15.0	12.0	8.0	2.0	-9.0	-10.0		
	63.	74.	90	100	120	140.		
446	15.0	8.0	7.0	-1.0	-8.0	-11.0		
	70	83	90.	100	120.	140.		

* There are old Piles Elev: 16.7 bet: Sta. 446+15 + 446+85
3 rows 10' apart + 8' apart
East + West.
These rows are 60' 68' + 76' out.

442+31	9.0	3.0	-2.0	-10.0	-12.0			
	75	90.	100.	120.	140.			
442	15.0	13.0	11.0	8.0	4.0	-6.0	-11.0	-13.0
	56	65.	75.	80.	90.	100	120	140.
+50	15.0	13.0	8.0	6.0	4.0	-1.0	-7.0	-11.0	-12.0
	53.	64.	70.	75.	80.	85	95.	120.	140.
441+35	15.0	13.0	11.0	8.0	4.0	1.0	-7.0	-11.0	-12.0
	52.	60.	70.	75	80.	85	100	120.	140.
440+85	15.0	11.0	10.0	5.0	-3.0	-6.0	-11.0	-13.0
	66.	77.	80.	85.	95	100.	120.	140.

X Sections opp: Retaining Wall at Gas Works.

Sta.	Grade Elev.	Left				Right
	33.20					
+25	Near Stand Pipe	-5.4 67	-5.2 54	-6.0 46	-1.9 20	0.0 6
18+00	To Oil Tank	-6.2 60	-6.2 46.	-6.4 32.	-4.1 20.5	0.0 4.0
17+74.	To Oil Tank	-7.2 50.4	-6.9 39.4	-7.0 20.5	-3.5 12.	0.0 9.0
+50		0.0 20.5	-6.5 20.5	-5.0 14.	-1.8 12.	0.0 8.0
17.		0.0 20.5	-7.0 20.5	-4.1 13.	-1.5 11.5	0.0 8.0
16+75		0.0 20.5	-7.6 20.5	-5.9 15.	-1.6 13.5	0.0 8.0
+50		0.0 20.5	-7.3 20.5	-7.3 17.5	-2.8 14.	0.0 9.
+25		0.0 20.5	-6.7 20.5	-5.1 17.		0.0 10.5
16		0.0 20.5	-7.4 20.5	-5.5 17.	-1.4 15.	0.0 11.5
15+75		0.0 20.5	-7.2 20.5	-5.5 17.5	-0.7 14.	0.0 11.
15+50		R Wall 0.0 20.5		-7.0 20.5		0.0 12.
15+31		R Wall 0.0 20.5		-7.4 20.5		0.0 13.

Pages 24 To Used In
Final Estimate Item No 9

1413

X Secs. of Merkley Borrow Pit.

	Base Line												
3	14.0	18.6	19.5	20.3	21.7	23.8	23.4	21.9	21.9	19.7	19.6		
		17.	18.	22.	23.	40.	61.	90.	119.	142.	150		
2 + 75	15.3	18.7	19.3	20.3	21.9	23.4	23.0	22.6	20.9	19.9	19.8	20.7	20.8
		18.	19.	24.	25.	45	65.	75.	117.	129.	139.	145.	147.
2 + 50	15.1	17.4	20.3	21.7	23.1	22.5	22.6	21.0	19.7	19.7	21.1	20.8	
		22.	22	24.	46.	64.	84.	100.	122.	133.	143.	147.	
2 + 25	15.8	18.6	19.7	20.5	21.3	23.5	23.4	19.3	19.5	21.0	20.9		
		17.	18.	23.	25.	60	70.	118	130	138.	149.		
2 + 00	15.7	17.2	18.6	19.6	20.3	21.2	23.9	23.7	22.9	22.3	20.2	18.9	19.1	20.9	20.9
		4.	14.	15.	20.	21.	41.	52.	71.	83.	96.	119.	127.	150	137.
1 + 75	17.9	20.3	21.2	23.5	22.6	21.9	20.0	18.9	19.3	20.2	20.0				
		17.	18.	42.	65.	78	93.	115.	124.	128.	136.				
1 + 50	17.3	19.7	20.3	21.1	23.1	22.5	21.9	20.3	20.6	20.2	20.6				
		20.	15.	16.	36.	57.	75	100.	116.	128.	136.				
1 + 25	18.1	18.7	19.5	21.7	22.8	22.4	21.4	20.1	20.0	20.7	21.8	21.7	
		6.	7.	27.	44	53	75.	95	109.	130	135	141.	
1 + 00	17.5	18.1	18.3	17.6	21.9	22.4	21.9	20.9	19.6	20.3	20.5	21.7	22.9
		1.	22.	32.	44.	53	64.	75.	100.	108.	123	130.	150
0 + 75	17.8	17.7	16.5	16.1	16.7	19.1	20.3	21.4	21.1	20.1	20.0	20.9	23.3
		6.	13.	24.	42.	46.	60.	65.	75.	83	93	119.	148.
0 + 50	18.2	17.9	17.4	18.2	19.9	20.0	20.1	21.0	24.3	27.3			
		18.	22.	47.	64	75.	100.	110.	133.	150.			
0 + 35	19.7	18.6	21.0	20.9	19.5	20.3	22.7	24.6					
		38.	40.	52.	75.	96.	118.	130.					
0 + 15	20.1	19.7	21.3	21.0	19.6	19.7	22.1						
		28.	30	42	64	75.	105.						
0		no grading						0.0					

BM. 21.00 near Sta. 0 on poplar stump

X Secs. of Merrifield Borrow Pit.

S 1/2.

Base Line

For X Secs for Estimate see pp. 47-48.

5+00	13.4	15.8	17.9	18.9	20.0	22.8	22.8	22.1	22.4	End of Pit	
		7.	13.	19.	21.	52.	72.	116.	150		
4+75	12.8	15.2	16.8	18.8	19.8	22.2	22.9	22.3	22.1	22.3	22.5
		7.	9.	21.	22	39.	55.	92.	115.	139.	150
4+50	11.9	12.9	16.4	18.9	19.9	22.2	23.1	22.1	22.5	22.3	
		4.	8.	22	23.	41.	53.	100.	145.	150.	
4+25	9.9	16.5	18.4	20.9	22.7	23.2	22.7	22.0	22.2	21.8	
		10.	20.	28.	44.	54.	75.	115.	147	150.	
4+00	9.5	14.8	18.6	19.7	20.3	21.2	23.3	23.7	22.4	22.3	20.7	20.6
		7.	23.	24.	27.	28.	46.	55.	100.	142.	148.	150.
3+75	10.4	14.0	17.5	20.2	21.5	23.7	23.4	22.4	22.3	21.4	
		5.	15.	27.	30.	48.	67.	86.	139.	143.6	
3+50	11.9	13.9	17.7	20.4	21.4	23.9	23.2	22.8	22.5	22.5	21.1	20.2
		3.	14	27.	28.	44.	69.	100.	108.	132.	138.	145.3
3+25	13.4	15.8	18.7	19.7	20.5	21.7	24.0	23.6	22.1	20.0	19.3
		6	18.	19.	24.	25.	44.	64.	122.	139.	147.

Copied 11/18/27 CCB.

X Sections on Co. Road Road 30' wide
Grade Sta. 149+60. 1-1 Slope

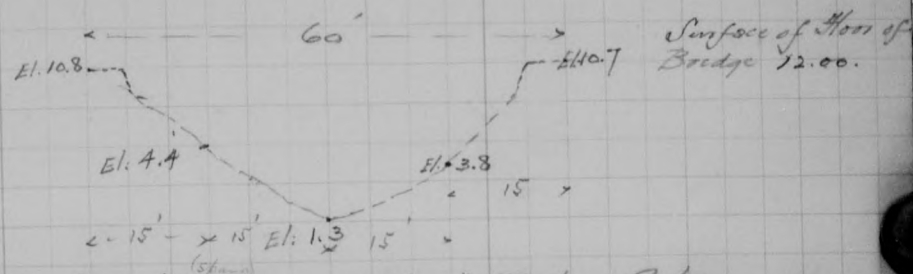
2+40	25.237		0.0 15.0		0.0		+0.2 13.	+1.4 16.4			
2+00	22.837		+0.4 15.4	+2.1 5.	+2.3			+2.8 17.8			
1+50	19.837	+4.8 19.8	+5.0 17.	+2.7 13.	+2.6 9.	+4.0 5.	+4.7	+4.4 19.4			
1+00	16.837	+7.6 22.6	+7.0 18.	+6.5 14.	+4.1 11.	+4.1 4.	+5.3	+6.0 5.	+5.7 20.7		
0+75	15.337	+8.5 23.5	+7.2 13.	+5.8 9.	+5.0 4.	+5.7	+6.4 6.	+6.4 21.4	+6.6 30.0	1/2-1	
0+50	13.837 1/2-1 Slope.	+7.6 31.4	+8.8 23.8	+9.4 19.	+8.4 12.	+6.3 8.	+6.4		+7.0 22.0		1/2-1 +6.9 29.4
0+25	13.837 1/2-1 Slope	+7.4 38.2	+7.3 22.3	+7.3 16.	5.4 8.	+5.8	+5.6 13.	+5.8 20.8	+12.8 40.0	1/2-1	
Sta. 149+60 = 0+00.	13.837 1/2-1 Slope		+4.2 48.6	+4.7 19.7		+4.5		+4.4 9.	+5.1 20.0	+7.5 28.	+8.2 1/2-1 47.1
0+25 West	13.837 1/2-1 Slope	+6.3 34.1	+6.0 21.0	+6.0 18.	+4.4 12.	+2.9 9.	+2.6		+3.1 9	+2.6 17.6	+3.0 1/2-1 31.1 Slope
0+50				+2.6 17.6	+1.4 11.	+1.0		+1.0 16.0	+0.7 28.3	1/2-1 Slope	
0+69				0.0 15.0		0.0		0.0 15.0			

Level

F.M.J. 6-12-12

X Section of Slough at Klotz Ranch.

Klotz to be provided with following Bill of Lumber to build bridge for farm purposes, in place of grading Crossing under Trestle at Sta. 328 +.



Bridge to be 20' bents.
14 feet wide.

8"x8" Posts & Caps
2"x12" Sm. Braces
3"x12" Floor.
3"x16" Stringers. 2' Centers

Bill of Lumber

✓ 2 Sills 8"x8" - 14 R.W.
✓ 2 Caps 8"x8" - 14 ~~R.W.~~ O.P.
✓ 6 Posts 8"x8" - 10' R.W.
24 Stringers 3"x14" - 20.
✓ 2 Sills 8"x8" - 14. R.W.
~~32~~ 3"x12" - ~~4~~' (midsills), R.W.
4 Sm Braces 2"x12" - 18 Pine
~~54~~ 60 pcs 3"x12" - 14 (Flooring) Pine 6-18
12 pcs 4"x4" - 4 pine
6 " 2"x4" - 20 pine
6 " 2"x6" - 20 pine
12 lbs 60 Nails
16 lbs 20 Nails

Oct 21st/07 32.

Sta: Orig: X Sec: of Miller Borrow Pit

2+10							18.0	17.4	15.7	15.0	15.7	16.0	15.4	15.4	18.4	19.0	20.4
							51.	47.5	44.	25.		4.	5.	17.	19.5	22.	24.
2						13.6	15.3	15.1	15.7	15.2	15.8	15.9	15.2	15.2	16.8	20.4	
						79.	60	54.	40.	30.		3.	8.	17.	18.5	24.	
1+80					11.5	13.5	15.7	15.6	15.3	17.3	17.5	17.7	15.8	15.7	19.6	22.5	
					93	79.	54.	32.	23.5	6.		6.	8.	22.	25.5	30.	
1+60		11.2	12.6	12.1	12.6	13.5	15.5	15.7	18.3	19.2	18.6	18.7	18.8	16.5	16.0	20.2	20.5
		124.	115.	110.	100.	85.	73.	50.	41.5	31.	14.5		6.5	10.	20.5	25.	29.
1+40		15.7	15.2	13.7	12.6	14.6	15.1	16.5	17.9	19.1	19.7	19.8	20.1	20.8			
		141.	139.	135.	118.	100.	90.	62.	37.	21.		12.	20.	25.			
1+20		15.2	15.3	13.5	13.5	15.1	15.8	17.1	18.5	19.6	20.2	20.0	20.8	22.0			
		153.	148.5	141.	119.	100	85.	55.	29.	21.		16.	26.	31.			
1+00		16.2	16.3	14.0	14.8	15.4	16.4	16.2	18.5	18.1	17.0	16.4	18.2	19.3	21.3		
		164.	143.	125.	100.	80.	47.	29.	22.	4.		12.	13.5	18.	22.		
0+80	18.7	16.7	16.8	16.2	14.5	14.2	14.9	15.1	16.0	16.7	16.6	15.9	15.9	15.0	18.4	20.1	
	170.	166.	161.	147.	129.	122.	100.	70.	41	25.5	4.	2.5	2.5	9	11.	16.	
add 8.5 x 8.5 x 4.5 for mound.																	
0+60.	19.4	18.6	14.7	14.2	14.9	14.8	13.6	14.7	15.3	15.0	15.7	16.0	16.4	16.7	15.4	15.2	15.2
	171.	168.5	165.	162.	154.	129.	113.	105.	100.	69.	51.5	31.	18.	5.	4.		11.
0+40	20.6	19.0	13.5	14.5	15.5	15.3	14.1	14.6	15.4	15.8	14.8	14.9	15.2	15.9	16.1	15.4	15.5
	179.	175	171.	155.	152.	134.5	131.5	121.	120.	100.	96.	82.	61.	30.	1.5		12.
0+20		18.5	17.6	14.1	13.8	15.1	15.7	14.6	15.0	15.3	14.4	15.5	16.1	16.7	16.5	18.5	20.2
		185.	179.	173.5	165.	147.	111.	100.	75.	48.	35.	17.	13.5		6.5	9.	14.5
0+10		15.5	20.0	14.5	15.3	20.2	20.5	20.2	15.0	15.5	16.9	16.9	16.7	20.1	20.7		
		100.	90.	81	63.5	51.	37.	31.	22.	15.5	11.		3.	6.	12.		
0+00												20.4					

1418

S/2 Orig: X Secs: of Miller Borrow Pit

	Elev:								
3+41.5 △	20.17								
3+30	15.5 18	17.1 7.5	18.6	19.3 3.	19.9 4.	20.5 6.5	20.7 10.		
3+25	15.5 19.	16.6 4.	17.1	17.4 4.	20.4 8.	20.5 12.			
3+20	15.3 20.	16.3 9.	16.3	16.8 9.5	20.5 12.	20.7 15.			
3	19.5 23.	19.5 22.5	14.7 19.	15.4	16.5 5.5	15.9 15.5	20.5 17.5	21.4 22.	
2+80	18.0 30	18.0 29.5	14.3 24.	15.8 8	16.0	15.9 8.	16.0 18.5	19.7 23	19.9 24
2+55	18.0 36.	17.7 35.	15.7 30.5	14.4 28.	15.9 22.5	15.2 10.5	15.9 8.	16.0	15.4 6.	19.3 8.	21.8 16.	22.5 24.
2+40	18.8 43.	14.9 38.	15.7 31.	15.4 16.	15.9	16.1 4.	15.3 7.	15.2 15.	20.7 18.5	21.9 24.
2+20	19.9 48.	18.2 47.	15.5 42.	15.5 24.	15.6	15.3 17.5	19.3 31.	20.9 24.	

Oct 29/07

35.

Sta: X Secs: County Road South of Y Street

Road 18' wide
Crown 2.5 in Center
Slope 1½ - 1.

	Grade Elev.									
2+00	14.30			-3.3 / 14.0	-3.6	-3.0 / 9.	-2.5 / 12.8			
1+80	15.40			-4.5 / 15.8	-4.9	-4.3 / 15.4				
1+60	16.60		-11.4 / 26.1	-10.4 / 20.	-6.1 / 9.	-6.1	-5.4 / 17.1			
1+50	17.20		-7.0 / 19.5	-8.8 / 8.	-8.9 / 2.5	-8.2	-7.0 / 2.5	-6.1 / 18.2		
1+46 Pipe 24"	- 42.5 long 17 Joints									
1+40	17.80		-6.8 / 19.2	-7.3 / 10.	-9.3 / 7.	-10.2	10.1 / 7.5	-6.7 / 9.	-6.6 / 18.9	
1+30	18.40			-7.4 / 20.1		-8.1	-8.8 / 3.	-11.5 / 5.	-12.8 / 15.	-10.2 / 18.	-10.3 / 24.4
1+19	19.06			-8.0 / 21.0		-8.6	-8.1 / 7.5	-11.6 / 21.5	-12.0 / 27.0	
1+00	20.20			-8.9 / 22.4		-9.6		-9.2 / 22.8		
0+50	23.70			-11.5 / 26.2		-12.2		-12.0 / 27.0		
0+40	23.80			-12.1 / 27.2		-12.8		-12.1 / 27.2		
0+20	25.00			-5.9 / 17.9		-6.0		-5.4 / 17.1		
0+06				-0.2 / 9.3		-0.2		-0.2 / 9.3		
0+00				0.0 / 9.0		0.0		0.0 / 9.0		

Level - 6.00

Pages 35 To 41 Used In
Final Estimate Item No 23

1420

Co Road S of Y SH

Sta:	Grade Elev.		L		C		R	
5+50			-1.7 / 11.6	-1.6 / 9.	-2.1	-1.6 / 9.	-1.6 / 11.4	
		add for Ditch 3' x 4.5' x 28' = 14 Cu. Yds.						
5		Level	-1.9 / 11.9.	-1.9 / 9.	-2.4	-1.9 / 9.	-2.0 / 12.0	
+50			-2.0 / 12.0	-2.0 / 9.	-2.5	-2.0 / 9	-2.0 / 12.0	
4			-2.3 / 12.4	-2.7 / 9.	-2.7	-2.0 / 9.	-2.0 / 12.0	
3+74			-4.1 / 15.2	4.9 / 9.	-4.4	-4.1 / 3.	-2.7 / 6.	-2.1 / 12.2
3+50			-4.6 / 15.9	-5.0 / 9.	-4.9	-4.7 / 9.	-4.1 / 15.2	
3+42			-3.9 / 14.9	-4.6 / 9.	-5.1	-4.6 / 9.	-4.5 / 15.8	
							16' opening	
3+26. EB			-4.6 / 15.9	-4.7 / 9.	-5.2	-4.8 / 9.	-4.6 / 15.9	
BM. 15.020.								
3+11.		Level	-4.0 / 15.	-6.0 / 9.	-5.4 / 4.5	-5.2	-4.6 / 9.	-4.7 / 16.0
3+00.				-1.7 / 11.6		-2.6	-2.7 / 2.	-8.0 / 15. -7.8 / 19. -7.3 / 20.0
2+80				-1.7 / 11.5		-2.2		-1.7 / 11.5
2+50	13.00			-1.2 / 10.8		-1.7		-1.5 / 11.2
2+20.	13.00			0.0 / 9.0		0.0	+0.9 / 7.	+1.5 / 10.5

Sta.	Grade	L.	C.		R.	
10 + 95		-0.7 / 10.0	-0.7 / 9.	-1.3		0.0 / 9.0
BM. 12.03 Iron Cor. Rt of 10+95						
10 + 50		-0.4 / 9.6	-0.4 / 9	-1.0	-0.6 / 9.	-0.5 / 9.8
10		-0.4 / 9.6	-0.4 / 9.	-1.0	-0.4 / 9.	-0.4 / 9.6
9 + 50		-1.1 / 10.6	-1.0 / 9.	-1.6	-1.0 / 9.	-1.0 / 10.5
9 + 10		-1.8 / 11.0	-1.2 / 9.	-1.8	-1.2 / 9.	-1.2 / 10.8
9.		-4.2 / 15.3	-4.5 / 9.	-2.3	-1.5 / 9.	-1.4 / 11.1
Box at 8+96. Elev. Bottom 6.7. " Top 11.0			Box 31.6' long.			
8 + 80		-1.9 / 11.9	-1.9 / 9.	-2.4	-2.0 / 9.	-2.1 / 12.2

Sta.	Grade	L.	C.		R.	
8 + 50		-1.2 / 10.8	-1.2 / 9.	-2.1	-1.6 / 9.	-1.5 / 11.2
8.		-0.7 / 10.0	-0.6 / 9.	-1.1	-0.5 / 9.	-0.6 / 9.9
7 + 50		0.0 / 9.0		-0.2	0.0 / 9.0	
7	Zero el.	-0.7 / 10.	-1.0 / 9	-1.4	-1.0 / 9.0	-0.6 / 9.9
6 + 50		-1.3 / 11.0	-1.2 / 9.	-1.7	-1.0 / 9.	-1.0 / 10.5
	add for Ditch 4' × 1.5 × 28 = 6.2 Cu. Yds.					
6	13.00	-2.2 / 12.3	-2.1 / 9.	-2.7	-2.1 / 9.	-2.1 / 12.2
	add for Ditch 2.5 × 3 × 25' = 6.9 Cu. Yds					

Sta.	Grade		L.		C.	R.	
17			-2.7 13.0	-2.8 9.	-3.2	-2.5 9.	-2.4 12.6
	+50	13.00	-2.0 12.0	-2.0 9.	-2.3	-1.7 9.	-1.7 11.6
16		25.00 Hub to Fence 15+94.5 25.00 Hub to Fence	0.0 9.0		-0.6		0.0 9.0
	+50		+0.8 9.8		+0.5	+2.0 10.0	0.0 14.3
15			0.0 9.0		0.0	+1.7 12.	0.0 14.3
	+50		0.0 9.0		-0.7	+0.3 9.	0.0 13.3
14			0.0 9.0		-0.3	+1.0 12.	0.0 14.3
	+50		-0.5 9.8		-1.0	+0.7 12.	0.0 13.9
13		25.00 Hub by Fence Post	-0.6 9.9		-0.9		0.0 9.0
	+55.4						
	+50	Hub by Fence Post	-0.7 10.		-0.8		0.0 9.0
12			0.0 9.0		-0.4	0.0 5.	+0.6 18.7
	+50		0.0 9.0		0.0	+0.7 9.	+1.2 20.0
11	13.00	25.00 RP 10+96.2 25.00 R.P.	-0.8 10.2	-1.0 9.	0.0	+0.4 9.4	

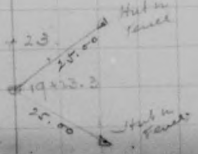
Sta.	Grade	L.	C.	R.		
+50		-1.1 / 10.6	-1.1 / 9.	-1.7	-1.1 / 9.	-1.2 / 10.8
21		-1.2 / 10.8	-1.3 / 9.	-1.7	-1.1 / 9.	-1.0 / 10.5

Add for Ditch at Sta: 20+65. 4' x 3' x 25' = 11.1 Cu: Yds.

20+65.5 24" Pipe ~~25'~~ 26.6' long 11 Joints

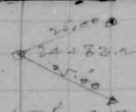
+50		-1.1 / 10.6	-1.0 / 9.	-1.6	-1.2 / 9	-1.2 / 10.8
20		-1.2 / 10.8	-1.1 / 9.	-1.5	-1.3 / 9.	-1.0 / 10.5
+50		-0.7 / 10.0	-0.7 / 9.	-1.3	-0.8 / 9.	-0.8 / 10.2
19		-0.9 / 10.4	-0.9 / 9.	-1.3	-0.7 / 9.	-0.7 / 10.0

BM 12.41 Fence Cor: 19+23.



18+50		-2.4 / 12.6	-2.1 / 9.	-2.2	-0.9 / 9.	-1.0 / 10.5
18+00 EB.		-3.3 / 14.0	-3.1 / 9.	-3.6	-3.2 / 9.	-2.9 / 13.4
17+84 EB		-3.0 / 13.5	-3.0 / 9.	-3.7	-3.2 / 9.	-3.3 / 14.0
17+50	13.00	-2.2 / 12.3	-2.0 / 9	-2.7	-2.3 / 9.	-2.4 / 12.6

Sta.	Grade		L.	C.	R.
+ 50	14.60		0.0 9.0	-0.5	0.0 9.0
27	14.40	+ 0.40	-0.3 9.4	-0.7	-0.2 9.3
+ 50	14.20		0.0 9.0	-0.6	0.0 9.0
26	14.00		0.0 9.0	-0.4	0.0 9.0
+ 75	Box 18" x 24" - 24' long				
+ 50	13.50	+ 0.50	0.0 9.0	-0.4	0.0 9.0
25.	13.00		-1.0 10.0	-1.2	0.0 9.0
+ 53	Box 18" x 24" - 22' long				
24 + 50			-1.2 10.8	-1.7	-1.9 6 -1.8 11.7



BM. 11.45 in Fence R. of 24 + 50

24		-1.8 11.7	-1.9 9.	-2.2	-1.3 9.	-1.3 11.0	
+ 50	Level L.	-3.2 13.8	-2.7 9.	-2.9	-2.1 9.	-2.1 12.2	Box at 23+50. 18" x 24 - 22'
23.		-1.1 10.6	-1.1 9.	-1.8	-1.2 9.	-1.1 10.6	
+ 50		-0.9 10.4	-0.9 9.	-1.6	-1.2 9.	-1.2 10.8	

24" Pipe 10 Joints

Pipe 25' Ex. Bott 8.9 add for Ditch at Sta: 22 + 23. 3' x 3' x 20' = 6.7 Cu. Yds.
" 8.5

22	13.00		-0.3 9.4	-0.9	-0.4 9.6

Sta.	Grade	Tu.		C.		R.
+ 35	End of Road	0.0 9.0		0.0		0.0 9.0
30		0.0 9.0		0.0		0.0 9.0
+ 50		0.0 9.0	0.0 4.	- 0.2	0.0 5.0	+ 0.4 9.4
29		0.0 9.0		- 0.6	0.0 7.0	0.0 9.0
+ 50	15.00	- 0.2 9.3		- 0.6		0.0 9.3
28	14.80	- 0.2 9.3	- 0.2 5.	- 2.2	0.0 7.	0.0 9.0

Dec 2nd/07 42.

Sta. X Section of Miller Borrow Pit for Estimate.

Sta.																		
2+20								19.9	17.7	15.1	11.0	10.3	10.7	10.8	11.8	19.3	20.9	
								48.	45.5	43.5	37.	22.		11.5	16.5	21.5	24.	
2+10								18.0	17.6	17.4	10.6	10.5	10.9	11.1	11.9	19.0	20.4	
								51.	49.5	44.	39.	17.		13.	17.	22.	24.	
2+00						13.6	15.3	13.9	12.6	11.5	10.4	11.3	11.6	12.9	19.9	20.4		
						79.	60.	59.5	54.	44.	23.		14.	18.5	22.	24.		
1+80							10.7	10.7	12.1	12.1	12.0	12.7	13.1	15.5	19.5	22.5		
							93.	83.	63.	47.	21.		17.	25.	28.	30.		
1+60			11.2	13.3	12.0	10.2	10.8	14.2	12.8	14.7	15.2	14.6	14.6	15.9	20.1	20.5		
			134	118.	115.	106.	85.	56.	38.	11.		9.5	18.	24.5	26.5	29.		
1+40	15.7	15.2	12.5	12.1	10.9	10.6	11.7	15.1	16.5	17.9	18.4	17.1	16.9	16.5	19.0	20.6	20.8	
	141.	139.	135.	133.	130.	119.	100.	90.	62.	37.	24.	10.		7.	21.	23.	25.	
1+20	15.2	15.3	12.3	10.8	11.7	13.9	15.1	15.8	17.1	18.5	17.5	16.0	16.1	15.9	18.2	20.6	22.0	
	153.	148.5	142.	137.	119.	107.	100.	85	55.	24.	14.	13.		10.	15.	18.5	31.	
1+00	16.2	15.9	14.3	11.8	12.9	13.4	14.8	15.4	16.4	16.9	16.0	14.8	14.4	13.9	14.5	16.2	18.8	21.3
	164.	158.	148.	144.	118.	107.	100.	80.	47.	41.	28.	17.		4.5	10.	11.5	18.	22.
0+80	18.7	16.7	16.8	13.2	11.5	9.5	9.8	10.0	10.9	14.5	15.3	14.9	13.2	13.3	14.3	19.4	20.1	
	170.	166.	161.	154	151.	131.	120.	100.	83.	53.	32.	17.		4.5	9.	13.5	16.	
0+60	19.4	18.6	14.7	14.2	11.4	10.4	9.7	9.8	10.8	15.2	15.2	14.7	14.2	13.5	13.3	14.2	16.0	22.0	22.9
	171.	168.5	165.	162.	158.	151.	129.	95.	78.	43.	31.	18.	5.		4.5	11.	13.5	18.5	20.
0+40			20.6	19.0	13.5	11.9	9.5	9.8	10.7	13.1	15.1	15.6	13.7	13.5	13.6	16.1	17.5	22.0	23.3
			179.	175	171.	161.	120.	100.	78.	47.	35.	25.		4.	9.5	16.	19.	22.5	27.
0+20			18.5	17.6	14.1	12.2	9.8	11.1	13.4	16.0	15.6	15.6	15.9	17.4	20.6	21.2		
			185.	179.	172.5	162	126.	67.	40.	24.	8.		5.	11.	15.	18.		
0+10																		
0+00																		

Bal. 0+60 + 0+80 add for Mound 8.5 × 8.5 × 4.5 = 12.04 Cu. Yds.

Orig: X Sec: 16.9

Orig: X Sec: 20.1

Calc. C.D.

for Orig: X Secs: see pp. 32-33 this Book.

14271

Sta 2: X Sec: of Miller Borrow Pit for Estimate

Decr 2/07 43.

3+30	Orig: X Sec. no grading done											
3+25				15.5 19.	16.0 8.	16.4	16.7 4.	18.3 6.	20.4 8.	20.5 12.		
3+20				15.3 20.	15.8 9.	15.6	15.7 6.5	17.3 10.	20.4 13.	20.7 15.		
3			19.5 23.	14.4 19.	12.3 17.	12.0	12.8 13.	15.1 15.5	20.7 18.5	21.4 22.		
2+80				18.0 30.	10.3 21.	10.0	10.1 8.	11.1 12.	12.3 16.	15.0 20.	19.1 23	19.9 24.
2+55		18.0 36.	17.5 33.	11.3 28.5	10.6 25.	10.0 24.	10.1	10.2 8.	11.0 13.	12.3 13.5	13.4 16.	15.5 18.	22.5 22. 22.5
2+40	18.8 43.	14.9 38.	13.9 36.	11.0 31.	11.0 29.	10.3 28.	10.3	10.3 7.5	12.0 15.	21.4 20.5	21.9 24.	

Dec. 6/07 47.

X Sec. of Medley Borrow Pit for Estimate

	Base Line													
3+00	14.0	13.6 6.	13.6 20.	14.5 50.	15.9 76.	17.5 102.	17.7 130.	20.2 135.	19.6 150					
2+75	15.3	13.3 3.	13.1 21.	13.6 41.	14.4 61.	15.9 77.	17.1 108.	17.5 130.	19.8 136.	20.8 147.				
2+50	15.1	13.3 6.	13.9 35.	12.8 40.	14.5 60.	15.6 79.	17.1 111.	18.1 115.	19.8 134.	20.5 138.	20.8 147.			
2+25	15.8	13.4 6.	12.8 13.	13.7 34.	14.8 62.	16.1 105.	21.0 138.	20.9 149.						
2+00	15.7	14.4 4.	13.9 18.	14.8 38.	15.0 48.	16.1 62.	16.6 115.	20.8 138.	20.9 156.					
1+75	17.9	16.5 4.	16.0 13.	17.2 27.	16.7 57.	17.4 87.	16.9 127.	17.5 131.	20.0 134.	20.0 136.				
1+50	17.3	19.0 10.	20.4 20.	20.5 50.	19.5 61.	20.8 75.	18.1 100.	16.6 133.	17.1 139.	20.3 133.5	20.6 136.			
1+25	18.1	18.9 6.	19.5 7	21.7 27.	22.5 44.	22.4 53.	21.4 75.	21.0 85	18.8 89.	17.5 100.	16.7 115.	18.6 138.	20.9 133.	21.7 141.
1+00	17.5	18.1 1	16.9 23	17.6 32.	21.0 44.	22.4 58.	21.7 64.	20.8 73.	18.4 80.	18.1 100	18.6 120.	21.4 131.	22.4 150.	
0+75	17.8	17.7 6.	16.5 13.	16.1 24.	18.7 42.	19.1 46.	20.3 60.	21.2 68.	18.7 80	20.3 104.	19.8 116.	21.1 125	23.3 148.	
0+50	19.7	18.6 38	21.0 40	20.9 52	19.5 75	19.7 96	20.1 110	21.0 123	22.3 143	21.3 150	=			
0+35	Orig: X Sec:													= the same as original.
0+15	Orig: X Sec:													
0+00	no Grading													

Dec 6/07 48.

X Sect. of Merkley Borrow Pit for Estimate

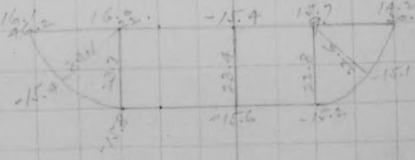
5+00 Orig: X Sec:

4+75	12.8	15.3	16.8	18.8	19.8	20.8	21.4	20.8	21.8	22.3	22.1	22.3	22.5	
		7.	9.	21.	32.	27.	35.	52.	73.	92.	115.	129.	150.	
4+50	11.9	13.9	16.4	18.9	20.3	21.4	22.7	22.1	21.9	22.6	22.1	22.5	22.3	
		4.	8.	24.	28.	37.	46	50.	70.	75.	100.	145.	150.	
4+25	9.9	16.5	18.4	19.6	19.4	21.1	21.3	22.4	22.0	22.2	21.8			
		10.	20.	34.	44.	64.	85.	90.	115.	147.	150.			
4+00	9.5	14.8	17.8	18.3	18.7	20.8	21.2	21.1	22.1	22.3	20.7	20.6		
		7.	18.	35.	56.	81.	100.	113.	130	142.	148.	150.		
3+75	10.4	14.0	17.1	18.0	17.8	19.1	20.8	22.0	21.5	22.4	22.2	21.4		
		5	13.	24.	44.	64.	80.	100.	118.	130.	139.	143.6		
3+50	11.9	13.9	16.2	16.7	17.5	19.2	21.4	20.9	21.5	22.6	21.1	20.2		
		3	10.	27.	31.	63.	104.	118.	137.	138.	138.	145.3		
3+25	13.4	15.8	14.8	16.0	16.2	17.6	18.0	19.4	20.7	19.3				
		6	8.	32.	52.	85.	97.	115.	130.	147.				

for orig X Sect. see pp 26-27.

additional X-sec.: See X Sec. Book 0-208. page 30 50.

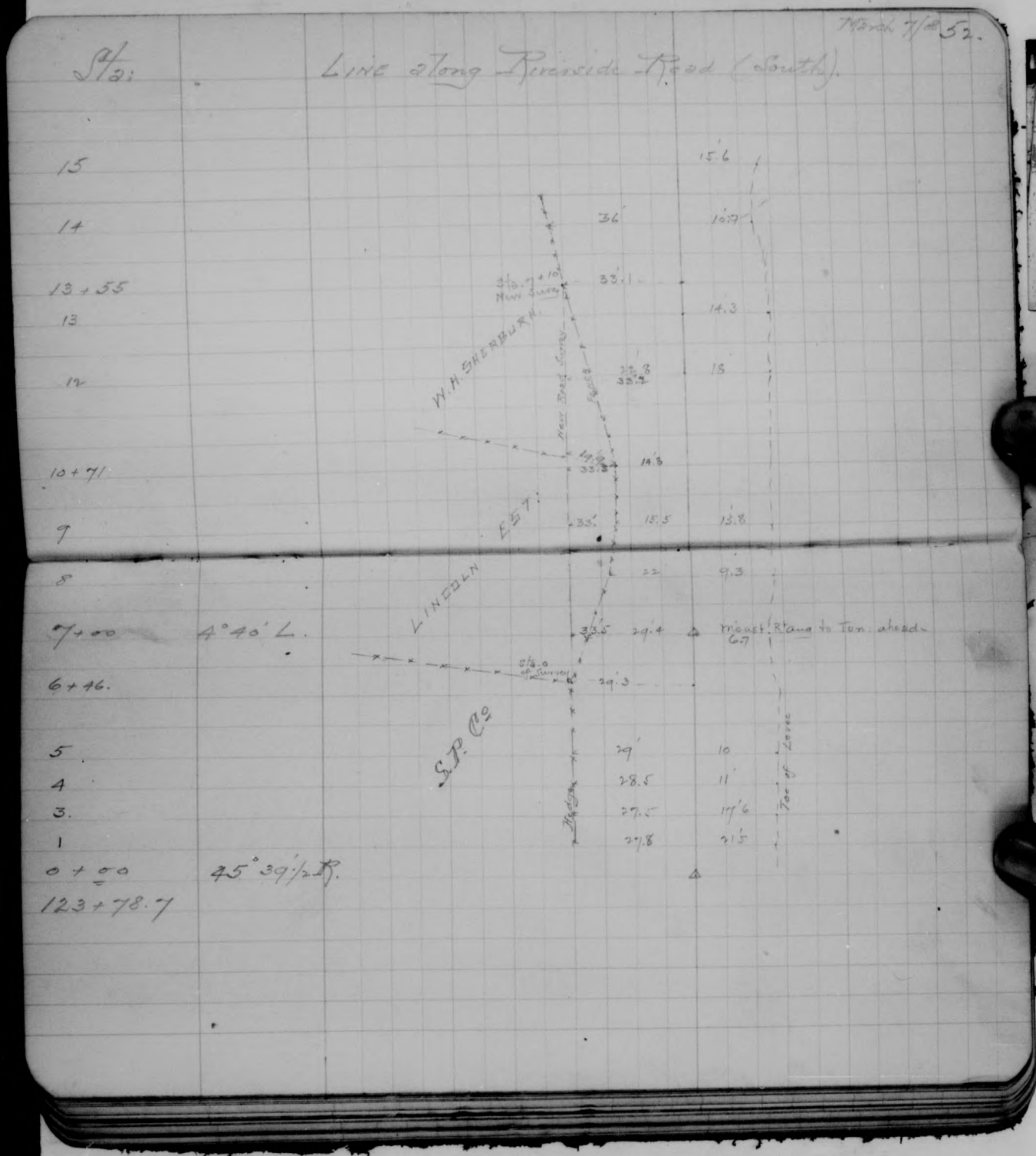
Sta.	from	L.	C.	R.
121+74		Crest old level -4.8 104.	-8.7 92.	-12.6 70.	-13.1 41.6	-13.9 22.	-14.7	-15.2 9.	-15.0 31.6	Top 13.1 78.	Crest level 0.0 105
121+50		Chimney Hole 30 -13.7 89.5	-13.8 84.5	-13.8 75.	-15.0 44.5	-14.9 22.	-15.3	-15.3 9	-15.1 31.6	Top 13.7 71.	Crest level 0.0 101.0
121+34		Crest old level -4.1 122	-13.3 104.	13.5 75.	-15.3 45.	-15.0 22.	-15.3	-15.3 9.	-14.6 30.9	Top 13.2 66.	Crest level 0.0 98.
121+06	-4.8 146.	-12.6 110.	-11.5 100.	-11.6 77.	-14.6 66.	-16.2 46.3	-16.1 23.	-15.6	-15.0 9.	-14.6 30.9	Top 13.6 61.	Crest level 0.0 91.5
120+97 E.B.	-5.4 137.5	-13.5 89.	-11.7 78.	-15.7 66.	-16.1 Alone	16.3	-15.4	15.7	14.2 30.3	Top 13.5 47.	Crest of level 0.0 88.0



120+75	Hty line	-6.2 93.	-7.6 82.	-8.6 79.	-16.0 50.
120+50				= 0.0 50.	Gas mott. Hty line

March 7th 52.

Sta: Line along Riverside Road (South).



S/2.

X. Sections on Riverside - Road. (South).

	L.		C.	R.	
12	Ditch 17.2 / 16.6	18.4 / 8.5	Road 18.1 / 6.	18.0	18.2 Toe / 18.
11	Ditch 17.4 / 9.5	18.4 / 4.8	Road 18.4 / 2.5	18.3	18.4 Toe / 18.7
10	Fence 18.6 / 13.0	18.9 / 4.	Road 18.6 / 2.5	18.3	18.3 Toe / 16.8
9	No Ditch Fence 18.6 / 15.5		Road 18.5 / 6.7	18.3	18.6 Toe / 13.8
8.	Ditch 17.9 / 19.5	18.8 / 11.5	Road 18.6 / 9.	18.6	19.0 Toe / 9.3
7	Ditch 18.0 / 25	19.0 / 21.	Road 18.6 / 14.5	18.6	19.1 Toe / 6.7
6	Ditch 17.9 / 25.3	18.8 / 21.	Road 18.6 / 12.5	18.7	18.8 Toe / 10.0
5	Ditch 17.3 / 24.5	18.3 / 19.	Road 18.7 / 14.	18.8	19.1 / 10.0
4	Ditch 17.7 / 23.	18.8 / 17.5	Road 19.0 / 13.	19.0	Toe 19.4 / 11.0
3	Ditch 18.3 / 25		Road 19.1 / 15.6	18.9	Toe 19.4 / 17.6
2	Ditch 18.0 / 23.4	18.7 / 17.	Road 18.8 / 12	18.8	19.1 / 15.4 — Toe 18.9 / 18.7
1		18.8 / 23.		18.8	18.9 / 18. — Toe 18.4 / 21.5
0 + 50	abut. 18.8 / 22			19.0	19.0 / 18.5 — Toe Levee 18.6 / 22.3
0 + 00				18.9	

E123 + 78.7 Cent Riv: Road

S 9/3

X Secs. on Riverside Road (South)

15		Ditch	Road			Toe
	no fence	17.1	17.9	18.3	18.1	17.9
		37.5	18.5	6.0		15.6
14	Fence	Ditch	Road			Toe
	17.0	17.1	17.8		17.9	17.8
	36.0	30.5	22.5			10.7
13		Ditch	Road			Toe
		17.2	17.8		17.9	17.8
		22.5	15.			14.3

123+ To 135

Ditch To Drain Riverside Road 2' Wide 1:1 Slope

7		14.30		+1.7 / 2.7	+1.8	+1.8 / 2.8
	+50	14.45		+1.9 / 2.9	+1.9	+1.9 / 2.9
6		14.60		+2.3 / 3.3	+2.4	+2.3 / 3.3
	+50	14.75		+2.4 / 3.4	+2.5	+2.5 / 3.5
5		14.90		+2.8 / 3.8	+2.8	+2.8 / 3.8
	+50	15.05		+2.8 / 3.8	+2.9	+2.9 / 3.9
4		15.20		+2.7 / 3.7	+2.7	+2.6 / 3.6
	+50	15.35		+1.7 / 2.7	+1.9	+2.0 / 3.0
3		15.50		+2.3 / 3.3	+2.9	+2.3 / 3.3
	+50	15.65		+2.3 / 3.3	+2.3	+2.3 / 3.3
2		15.80	0.30	+2.4 / 3.4	+2.3	+2.5 / 3.5
	+50	15.95	1	+2.3 / 3.3	+2.1	+2.3 / 3.3
1	+00	16.10		+3.1 / 4.1	+3.0	+3.1 / 4.1
	+75	16.17		bott. pipe (+75)- - - - - Pipe ends. 3.1 / 4.1	+3.0	12 Lengths 18" Vit. pipe 3.0 / 4.0
	+50	16.42		" " Pipe begins. 16.18 = Elev. bot. concrete.		
0	+00	16.58				
B.M. 18561						

FMY. 5-21-12

Pages 53 To 56 Used In
Final Estimate Item No 45

1435

Ditch - Riverside Road.

+50	13.25	0.0 1.0	0.0	0.0 1.0
10	13.40	+0.4 1.4	+0.3	
+50	13.55	+0.8 1.8	+0.7	+0.7 1.7
9	13.70	+0.7 1.7	+1.1	+1.1 2.1
+50	13.85	+1.4 2.4	+1.7	+1.5 2.5
8	14.00	+1.6 2.6	+1.6	+1.6 2.6
7 +50	14.15	+1.7 2.7	+1.7	+1.5 2.5

F.M.Y. 5-21-12.

S/2

X Sections on proposed site of Freeport Wharf. March 15th/09. 57.

	L.					C.						
379+50	26.7	26.6	22.5	19.7	17.8	S.W. 15.7	11.7	6.5	3.0	0.7	-1.3	-2.3
		7	30.	54.	57.	69.	80.	90	95.	100.	105.	110.
379	27.1	26.8	21.9	19.5	17.9	S.W. 15.7	9.7	9.5	3.0	1.7	-0.3	-2.3
		5.	31.	54.	67	71.	85.	90	95.	100.	105.	110.
378+50	26.9	26.8	23.6	22.5	18.2	S.W. 15.7	11.7	3.7	2.7	-2.7		
		6.	28.	50.	71.	74.	85	95.	100.	105.		
378	26.9	26.7	25.4	23.6	19.6	S.W. 15.7	13.7	6.7	5.7	2.7	-2.3	
		6.	17.5	25.	63.	74.	80.	90.	95	100.	105.	
377+50	26.5	26.5	21.6	18.9	15.7	S.W. 11.7	7.7	4.7	-0.3	-2.3		
		6.	37.	64.	71.	80.	90.	95.	100.	105.		
377	27.3	27.0	23.4	22.6	18.4	S.W. 15.8	8.8	4.8	1.8	-2.2		
		10.	32	45.	65.	71.	80.	90.	100	105.		
376+50	27.2	27.1	24.7	21.7	19.9	19.0	S.W. 15.8	11.8	6.3	3.0	1.8	-2.0
		10.	37.	42.	48.	54	57.5	70.	80.	90.	95	105.
376	27.1	26.8	23.4	21.7	19.1	S.W. 15.8	9.5	5.8	2.8	0.0	-2.2	
		10.	34.	37.	52.	46.	70.	80.	90	100.	105.	
375+50	27.1	27.0	25.3	16.9	15.8	S.W. 9.5	6.0	4.8	1.8	-2.2		
		11.	29.	41.	57.	70.	80	90.	100.	105.		
375	27.1	27.3	26.2	22.2	20.8	18.0	S.W. 15.8	9.8	5.8	1.8	-2.2	
		11.	30	36.	40.	42.	57.	70.	80.	90.	100.	
374	27.7	28.1	26.0	22.0	20.9	18.0	S.W. 15.8	5.8	0.8	-3.2		
		11.	33.	39.	43.5	46	61.	80.	90.	95.		
373	28.0	27.9	25.4	18.0	16.8	S.W. 13.8	3.8	-1.2	-3.0			
		11.	37.	48.	59.	70.	80	90.	95.			
372	28.4	28.7	29.5	26.1	17.9	S.W. 15.8	11.8	1.8	-3.1			
		8.	19	32.	46.	54.5	64.	80.	90.			

1437

Sta.

March 1st 09. 58.

X Sections on proposed Site of Freeport Wharf.

L. C. R.

opp. 370+50 B.M. 18.131.

" 381 B.M. 15.134.

383 + 50	27.2	26.7	23.7	18.6	17.2	14.6						
		9.	23.	34.	39.	61.						
383	27.0	26.9	25.0	20.0	17.7	14.6						
		9.	19.	31.	53.	82						
+ 50	26.7	26.1	24.5	21.6	17.0	14.6						
		9.	25.	32.	60.	76.						
382	27.1	26.9	19.9	17.7	15.7	9.0	7.0	6.0	1.7	0.7	-0.5	-2.0
		10.	34.	59.	72.	85	90.	95.	100.	105.	110.	115.
381	27.2	27.1	22.7	20.2	17.6	15.7	12.0	9.8	6.0	2.0	1.0	-2.5
		11.	38.	64.	69.	80.	85.	90.	95.	100.	105.	110.
380 + 50	27.1	26.9	22.3	20.3	17.4	15.7	9.8	5.0	1.7	-2.5		
		11.	36.	56.	63.	73	85.	95.	100.	105.		
380	26.9	27.0	22.4	19.9	17.7	15.7	9.8	6.0	4.7	2.7	0.0	-0.5	-3.3
		5.	34.	52.	55.	67.	80.	90.	95.	100.	105.	110.	115.

May 27/09 59.

S/3.

X Sections on Dold Site Freeport

372+50	C.R. Road Fence	15.3	14.8	14.5	17.5	(17.5 37.3) 17.8	27.4	27.4	27.4	26.0	15.2	12.7	S.N.	
		96	82.	72.	55.	42.5	22.5		10.	31.	51.	61		
373.	C.R. Fence	15.9	14.7	14.7	17.5	(17.5 39.3) 17.5	27.4	27.4	27.4	25.4	18.0	15.5	12.7	S.N.
		99.5	83.	71.	55	43.	22.5		10.	37.	48.	59.	64.	
373+50	C.R. Fence	15.3	14.7	14.9	17.5	(17.5 37.3) 17.7	27.4	27.4	27.4	24.8	20.1	15.2	12.7	S.N.
		102.5	86.	67.	55	43	22.5		10.	30.	48.	54.	64.	
374	C.R. Fence	15.7	14.9	15.8	17.5	(17.5 37.3) 17.6	27.4	27.4	27.4	26.0	22.0	20.9	18.0	15.8	12.7	S.N.
		102.5	82.	63.5	55.	41.5	22.5		10.	33.	39.	43.5	46.	61.	64.
374+50	C.R. Fence	15.5	15.7	17.4	17.5	(17.5 37.3) 17.8	27.4	27.4	27.4	24.0	20.5	15.3	12.7	S.N.
		100.	85.	66.	55	41.5	22.5		10.	31.	39.	49.	59.	
375	C.R. Fence	15.0	15.5	17.2	17.5	(17.5 37.3) 17.8	27.4	27.4	27.4	26.1	21.8	18.0	15.1	12.7	S.N.
		104.	77.	60.	55.	38	22.5		10.	24.	35	42.	46.	61.
375+50	C.R. Fence	14.8		14.5	15.8	17.5	17.7	27.4	27.4	27.4	25.3	16.9	14.4	12.7	S.N.
		108.		85.	68	55.	39.5	22.5		10.	24.	41.	45	57.	
375+92.7. Bott of House Track Grade.	C.R. Fence	14.8	15.2	15.5	17.5	(17.5 37.3) 17.8	27.4	27.4	27.4	23.9	20.1	19.5	16.7	12.7	S.N.
		109.	85.	62.5	55.	37.5	22.5		10.	37.	40.	46.	48.	58

* Readings in Brackets Give Toe of Slope as it ought to be when finished.

Reed Teaming Co. Force Work — Jan 3/08 — 63.

X Sec: of Borrow Pit for Estimate

Sta: — Dist. Line — FINAL X-Sects. Reed Co. Force Work

Sta.	Dist. Line										
+65		11.1	9.6	5.6	4.2	4.2	4.7	5.4	6.1	8.8	11.5
		4	7.	11.	20.	40.	69.	90.	109.	110.	114.
+50		11.3	7.4	5.6	4.4	4.2	4.5	5.3	6.4	11.4	
		4	10.	12.	17.	44.	80.	105.	108.	115.	
+33.		10.6	8.7	7.2	5.7	4.0	3.8	3.8	4.8	7.8	11.5
		4	8.	10.	11.	18.	37.	73.	102.	109.	115.5
+11.		11.4	9.8	5.6	4.1	3.9	4.2	4.7	9.1	11.8	13.0	15.3
		3	7.	11.	18.	30.	77.	100.	110.	115.	120	127.
338.		11.1	9.4	5.6	4.1	4.0	4.4	3.9	5.1	9.1	12.1	15.4
		4	7.	11.	18.	33.	75.	93.	102.	110.	115.	125.5
+92.		11.2	8.8	5.0	3.7	3.8	4.3	3.9	5.1	7.1	11.6	
		4	7.	11.	17.	36.	75.	97.	103.	107.	115.	
+50		11.1	8.9	4.7	3.6	3.3	3.7	4.5	5.7	7.9	11.1	
		4	8.	13.	18.	45.	78.	102.	105.	102.	114.	
+33		10.8	9.0	5.6	3.6	3.4	3.6	5.	6.2	7.7	11.2	
		4	7.	13.	20.	40.	75.	95.	106.	108.	113.	
+24		10.9	8.6	6.0	4.2	3.7	3.7	4.5	6.1	11.0	12.9	15.3
		4.	7.	12.	18.	30.	60.	100.	105.	111.	118	126.
+14		10.6	8.6	6.0	4.2	3.7	4.1	4.2	5.0	11.1	13.1	15.2
		4	7.	11.	14.	39.	73.	92.	105.	112	119.	126.
337		10.6	8.5	6.0	4.3	3.3	3.6	4.6	6.1	8.4	11.0
		4.	7.	11.	13.	24	60.	102	107	108.	114.
+50		10.6	10.0	7.9 (est.)	3.4	3.1	3.2	3.6	7.1	11.0	
		5.	8.	15.	30.	60.	100.	109.	114.		
336		10.5	10.4	9.2 (est.)	5.1	3.5	3.8	3.6	5.3 (est.)	6.4	8.7	10.6
		2.	6.5	12.	41.	70.	102.	107		109.	112.	113.
335+50		10.2	10.0	8.8	8.2	7.8 (est.)	6.0	5.5	6.0	7.6 (est.)	10.3
			5.	6.	30.	50.	58.	81.	105.	109	113.5

73 - 76

Pages 63 To 67 Used In Final Estimate Item 9

1440

Reed Teaming Co., Force Work

64.

St/2.

X Secs. of Borrow Pit for Estimate

FINAL

+85.	12.1	12.1	10.7	10.7	7.7	5.4	5.2	6.8	9.5	12.6			
	2	4	5.	6.	9.	17.	55.	90.	109.	115.			
+68.	11.8	10.4	6.1	5.1	5.1	6.4	7.5	9.4	12.5				
	2	6.	11.	17.	34	90.	103.	111.	114.				
+53	12.0	7.6	5.6	5.1	5.6	5.9	6.3	8.7	12.4				
	2	11.	11.	16.	44.	65.	92.	108.	116.				
+43	11.8	7.6	5.6	4.7	5.4	5.4	6.5	6.4	7.7	8.8	10.9	13.2	15.6 13.55 14.9
	3	10.	13.	16.	44.	58.	66.	90.	102.	105.	112.	115.	123.
+33	11.8	7.5	5.1	4.4	5.7	6.5	6.4	7.5	8.7	10.7	13.1	14.8	15.6
	3.	11.	13.	20.	56.	66.	95.	102.	105.	112.	115.	123.	127.
+25.	11.9	7.6	5.9	4.3	5.4	6.6	6.3	7.1	9.7	11.7			
	3.	10.5	11.	16.	58.	66.	91.	103.	111.	114.			
340.	11.8	7.8	5.6	4.0	5.1	6.2	6.8	8.1	9.8	12.2			
	3.	9.	12.	19.	50.	70.	100.	108.	112.	114.5			
+80	11.8	7.4	5.4	4.1	4.6	5.9	6.5	7.6	12.2				
	3.	10.	12.	17.	50.	70.	100.	106.	115.				
+68	11.8	7.5	5.7	4.0	4.4	5.7	6.9	8.2	13.0	13.9		17.1	
	2	10.	11.	17.	40.	70.	99.	105.	116.	122.		130.	
+60	11.9	7.6	5.6	3.9	4.8	5.7	6.2	7.6	13.7	13.8		17.0	
	3	10.	11.	18.	44.	78.	98.	105.	116.	122.		130	
+50	11.8	7.6	6.4	4.3	5.1	5.7	6.2	12.2					
	3.	10.	11.	22.	55.	86.	102.	114.					
339	11.4	9.4	7.9	6.3	4.5	4.1	4.8	6.5	8.3		11.7		
	3	7.	9.	10.	19.	40.	70.	105.	110.		116.		
+84	11.3	9.4	7.9	5.9	4.4	3.9	4.8	5.5	7.1	8.2	9.7	12.1	15.7
	3	7.	9.	11.	18.	35.	53.	83	106.	109.	110.	115.	127.5
338+75	11.2	9.6	7.5	5.8	4.6	4.1	4.6	5.9	6.5	8.7	10.0	12.9	15.4
	4	7.	9.	11.	18.	34.	45.	76.	105	110.	111.	116.	126.5

Reed Teaming Co. Force Work — Jan 3/08 — 65.

Sta. — X Sec of Borrow Pit for Est.

FINAL

Sta.										
+17	13.0 / 3	10.7 / 6.	7.3 / 14.	6.8 / 21.	7.0 / 45.	6.7 / 78.	7.8 / 99.	10.9 / 116.		12.9 / 118.
344	13.0 / 2	10.6 / 6.	7.0 / 14.	6.4 / 20.	6.9 / 45.	6.9 / 72.	8.6 / 100.	14.4 / 122.		17.2 / 129.
+89	12.7 / 3	10.0 / 7.	7.4 / 13.	6.4 / 20.	6.8 / 48.	7.3 / 77.	9.2 / 100.	12.1 / 109.	15.2 / 122.	17.5 / 127.
+73	12.8 / 3	10.0 / 6.5	7.3 / 13.	6.0 / 22.	6.7 / 45.	6.4 / 65.	8.0 / 95.	11.8 / 116.	12.3 / 117.	
+50.	12.5 / 2	9.5 / 7.	6.7 / 13	5.9 / 20.	6.5 / 43.	6.3 / 67.	6.8 / 92.	9.1 / 111.	12.5 / 117.	
343 +05	12.5 / 2.	9.1 / 6.5	6.3 / 14.	5.4 / 29.	6.6 / 46.	6.7 / 75.	7.7 / 100.	9.1 / 110.	12.5 / 117.	
+92	12.3 / 2	8.8 / 6.5	6.2 / 13.	5.4 / 35.	6.2 / 35.	6.6 / 72.	7.0 / 91.	8.3 / 101.	11.3 / 111.	15.6 / 122.	17.4 / 127
+84	12.1 / 3.	8.4 / 7.	5.6 / 14.	6.0 / 33.	6.6 / 69.	7.2 / 94.	8.0 / 102.	11.6 / 110.	12.2 / 122.	17.0 / 127.
+73	12.0 / 3.	8.3 / 7.	5.4 / 14.	4.2 / 28.	6.2 / 33.	6.6 / 77.	7.8 / 103.	12.5 / 117.		
+50	12.2 / 2	8.3 / 7.	5.4 / 14.	6.6 / 58.	7.6 / 105.	9.2 / 112.	12.5 / 116.			
342	12.3 / 2.	8.9 / 6.	5.6 / 13.	5.6 / 50.	7.3 / 95.	9.9 / 113	12.6 / 117.			
T.P. 12.35/15 at 341+15 +75	12.2 / 2.	8.3 / 7.	5.4 / 14.	5.7 / 50.	9.5 / 98.	12.8 / 115.	12.8 / 117.			
+50	12.3 / 3.	10.6 / 4.	6.5 / 11.	5.6 / 17.	6.5 / 61.	8.5 / 81.	11.5 / 114.	12.6 / 115	12.6 / 119.	
341	12.5 / 2	10.9 / 4.	7.6 / 11.	5.1 / 18.	5.6 / 45.	6.8 / 75.	7.8 / 100.	9.8 / 109.	12.5 / 114.	12.7 / 116.

Reed Teaming Co., Force Work — 7-24-4/28 — 66.

Sta: — X Secs. of Borrow Pit for Est.

FINAL

+30	14.9 / 3	11.2 / 8.	9.4 / 15	7.2 / 18.	6.1 / 27.	7.3 / 45.	8.2 / 85.	9.2 / 111.	15.1 / 120.	16.9 / 126.	18.7 / 133
+22	14.9 / 4	11.2 / 8.	9.5 / 15.	7.2 / 18.	6.2 / 27.	7.2 / 45.	8.2 / 86.	9.0 / 111.	10.8 / 112.	14.9 / 124.5	
347	14.5 / 4	11.3 / 8.	8.7 / 15.	6.8 / 22.	6.6 / 33.	7.1 / 65.	8.3 / 90.	9.4 / 112.	14.8 / 121.		
+58	14.0 / 3	10.0 / 10.	9.6 / 12.	8.4 / 14.	6.9 / 19.	6.4 / 37.	7.2 / 45.	8.3 / 90.	10.1 / 111.	14.5 / 120.	
+43	13.9 / 3	9.9 / 10.	9.2 / 12.	6.9 / 19.	6.8 / 32.	7.9 / 40.	8.1 / 81.	10.4 / 110.	13.4 / 115	15.3 / 124.	19.9 / 132.
+34	13.8 / 3	10.1 / 9.	8.9 / 13.	6.8 / 18.	7.3 / 35.	8.0 / 43.	7.8 / 81.	10.4 / 110.	14.5 / 118.	15.5 / 125.	19.6 / 131.
+20	13.6 / 3	10.4 / 8.	9.3 / 12.	7.0 / 18.	7.2 / 32.	7.3 / 75.	9.1 / 109.			13.2 / 117	
346	13.8 / 4	10.8 / 7.	9.8 / 10.	7.7 / 16.	7.0 / 19.	6.9 / 33.	7.4 / 90.	7.2 / 96.	8.7 / 109.	11.8 / 115.	13.8 / 118.
+60	13.2 / 3.	10.7 / 7.	9.5 / 10	7.8 / 14	7.1 / 18.	7.4 / 50.	6.9 / 63.	7.8 / 96.	10.3 / 110.	12.7 / 116.	
+46	13.6 / 3	10.9 / 7.	9.6 / 10	7.6 / 15.	6.9 / 19.	7.2 / 53.	7.8 / 89.	9.9 / 103.	13.9 / 110.	16.9 / 123.	18.2 / 131.
+36	13.4 / 3.	10.8 / 7.	9.5 / 10.	7.4 / 15.	6.8 / 18.	7.1 / 61.	8.0 / 95	9.4 / 102.	13.9 / 110.	16.6 / 123.	17.9 / 129.
+21	13.4 / 2	10.8 / 6.	9.4 / 10.	7.4 / 15.	6.8 / 18.	7.0 / 40.	6.8 / 60.	7.6 / 63.	7.7 / 100.	9.9 / 113	12.9 / 118.
345.	13.4 / 3	12.2 / 5	9.3 / 11.	7.0 / 17.	6.9 / 35	7.5 / 45.	6.8 / 85.	7.1 / 103.	8.9 / 111.	13.2 / 118.	
344 +50	13.0 / 3	10.0 / 8	7.2 / 16.	6.8 / 35.	6.1 / 53.	6.1 / 75.	5.9 / 94	9.9 / 115.	13.2 / 118.		

1443

Reed Teaming Co. Force Work — Jan 4/08. — 67.

Sta: — X Sect. of Borrow Pit for Est:

FINAL

Sta											
+80	0.0 runs out to grade.										
+50	16.1	15.5	13.6	13.5	10.2	9.4	9.7	11.1	15.0		
	2	5.	27.	41.	58.	83.	109.	115.	122.		
+38	16.0	15.2	14.4	10.6	9.4	9.0	9.7	11.7	15.0		
	3	7.	30.	50.	60.	89.	114.	116.	122.		
+20	15.9	15.2	14.5	10.6	9.3	9.2	10.3	15.0	16.6	17.5	
	4.	8.	25.	40.	76.	108	113.	120.	127.	131.	
+10	15.8	14.0	10.1	9.2	9.1	10.7	14.8				
	4.	21.	35.	72.	109.	115.	121.5				
349	15.9	14.1	10.0	8.7	9.0	10.2	14.9				
	4	14.	32.	86.	108.	115.	121.5				
+50	15.4	13.6	10.8	10.1	9.2	7.9	7.7	9.1	10.4	14.9	
	4	11.	14.	17.	19.	45.	80.	112.	115.	122.	
+43	15.5	13.6	10.5	10.1	9.0	7.6	8.6	9.4	10.4	15.5	16.1	19.2
	4	10.	14.	17.	20.	66.	88.	112.	115.	122.	126.	132
+34	15.0	13.1	10.3	8.3	7.4	8.1	9.3	10.3	15.2	16.5	19.2	
	7	11.	16.	21.	42.	80.	111.	114.	120.	128.	133.	
+22	15.3	12.0	9.8	7.5	6.6	7.7	8.6	9.3	11.1	15.1		
	5.	11.	16.	20.	37.	56.	94.	111.	116.	122.		
348	14.9	11.4	10.9	9.0	8.9	6.7	5.8	6.0	7.5	8.1	9.1	12015.2
	6.	10	12.	13.	15.	20.	28.	42.	60.	82.	111.	115. 121.
+50	14.9	11.1	9.5	7.1	6.6	6.1	7.1	8.0	9.2	14.9		
	4.	9.	14.	18.	20.	31.	47.	85.	110.	121.		
347 +43	14.8	11.1	9.4	7.1	6.0	7.6	8.1	9.9	14.6	16.7	18.4	
	4	9.	14.	18.	27.	50.	86.	111.	119.	126.	133.	